

HYDROGEOLOGICAL INVESTIGATION REPORT

Address

2-10 Berry Road, 14-16 Marshall Avenue & 5-9 Holdsworth Avenue, St

Leonards NSW

Prepared for

Holdsworth Land Pty Ltd

Reference No. E2670-4

September 2023

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DOCUMENT CONTROL REGISTER

Document Information					
Reference No.	E2670-4				
Document No.	1				
Report Title	Hydrogeological Investigation Report				
Site Address	2-10 Berry Road, 14-16 Marshall Avenue & 5-9 Holdsworth Avenue, St Leonards NSW 2204				
Prepared for	Holdsworth Land Pty Ltd				

Document Review Details						
Revision No.Issue DateDescriptionIssued By						
0	15/09/2023	Initial Issue	Ben Buckley			

Distribution Register						
Method Custodian Issued to						
Electronic	B. Buckley	Foundation Earth Sciences Office				
Electronic	T. Pizzolato	Holdsworth Land Pty Ltd				

Authorisation and Release						
– Signature Name Date						
Author ber buckley		Ben Buckley	15/09/2023			

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1.0 INTRODUCTION

Foundation Earth Sciences Pty Ltd was appointed by Holdsworth Land Pty Ltd to prepare a hydro-geological investigation report for the property located at 2-10 Berry Road, 14-16 Marshall Avenue & 5-9 Holdsworth Avenue, St Leonards NSW (hereafter known as the "site"). The purpose of this assessment includes:

- to achieve compliance with Council and Water NSW requirements in relation to the proposed future dewatering activities within the site.
- Assess the site surface and subsurface conditions and provide geotechnical recommendations for the design and construction of the proposed development.

Site	Details			
Location	2-10 Berry Road, 14-16 Marshall Avenue and			
	5-9 Holdsworth Avenue, St Leonards NSW 2065			
Lot/DP	Lots 38, 37, 36, 35, 34, 2, 1, 7, 8 and 9 Section 2 in DP7259			
Local Council	Lane Cove			
Area	Approximately 5,910m ²			
Shape & Slope	Irregular shape and gently sloping towards south east			
Existing Structures	Residential dwellings with associated structures			
Closest Watercourse	Berrys Creek is located approximately 350m west to the site			
Special Features	Holdsworth Avenue is located at least 3.0m below the all of the			
Special reactives	properties and there is a retaining wall along the road			
	North Marshall Avenue's road reserve and carriageway			
Neighbouring	East Holdsworth Avenue's road reserve and carriageway			
Properties	South Residential Type Properties			
	West Berry Road's road reserve and carriageway			
Coology Map	Sydney 1: 1:100,000 Geological Series Sheet 9029-9130 Edition 1,			
Geology wap	1983, from the Geological Survey of New South Wales			
Drimony Coology	Rwa – Ashfield Shale, Wianamatta Group, Triassic age, described as			
Primary Geology	"Black to dark-grey shale and laminite"			

Table 1: Summary of Details of the Site

Secondary Geology	Rh – Hawkesbury Sandstone, Wianamatta Group, Triassic age,
	described as "Medium to coarse-grained quartz sandstone, very
	minor shale, and laminite lenses" is located approximately 60m
	south west to the site
Proposed	Multi-storey building with five basement levels. Maximum
Development	excavation depth is inferred to be 17.0m

2.0 FIELDWORK AND LABORATORY TESTING

Following scope of work were carried out during the FES geotechnical investigation:

- Review of Dial-Before-You-Dig ("DBYD") plans and service locating.
- Mechanical drilling of four (4) boreholes, identified as BH1 to BH4 inclusive.
- Standard Penetration Testing ("SPT") within the augering of some of the boreholes.
- Installation of three (3) groundwater wells identified as GW1, GW2 and GW3 within the borehole BH1, BH2 and BH3 respectively.
- Subsequent visit to the site to measure the standing groundwater level.
- Laboratory testing of Point Load Index ("PLI") on the recovered rock samples.
- Laboratory testing of Aggressivity and Salinity on the soil and groundwater samples.

The approximate locations of the boreholes and groundwater wells are shown in a "Site Plan" and attached as Appendix A.

3.0 PROPOSED DEVELOPMENT

The site is currently occupied with residential dwellings including grassed areas, driveways, sheds and garages. The site is proposed to be redeveloped into a multi-storey residential building with multiple levels of residential units, three level basement car park, deep soil zone and landscape area. Maximum excavation depth is inferred to be approximately 17m BGL with an area of 1ha.

Refer to **Appendix G** – Proposed Development Plans.

4.0 GROUND CONDITION

4.1 Ground Profile

Ground profiles encountered within the boreholes are summarised in Table 2. However, reference should be made to borehole logs.

Unit	Details	Depth (m)			
Onit	Details	BH1	BH2	BH3	BH4
	Existing Ground Level (RL m AHD)	77.9	75.2	73.1	72.1
Fill	Gravelly Silt, low plasticity, fine to medium gravel, moist, firm Includes brick pavement	0.0-0.1	0.0-0.1	0.0-0.4	0.0 - 0.4
Residual Soils	Silty/Sandy CLAY, medium to high plasticity, moist, stiff-very stiff, interbedded of sandstone, shale	0.1 - 4.0	0.1 – 2.5	0.4 - 4.4	0.14 – 2.9
Class V ¹ Sandstone	SANDSTONE, interbedded with some clay and shale, extremely to highly weathered	4.0 – 5.7	2.5 – 4.9	4.4 - 7.0	2.9 – 6.2
Class IV ¹	SANDSTONE, with some shale	5.7 –	4.9 – 8.2	7.0 –	6.2 –
Sandstone	bands, moderately weathered	11.4		11.27	10.57
Class III ¹ Sandstone	SANDSTONE, with some shale bands, slightly weathered	11.4 - 8.2 17.75 17.98 -		-	

Table 2: Summary of Ground Profile

Note: ¹ Bedrock was classified in accordance with the research paper of Pells P.J.N, Mostyn G. & Walker B.F. Foundations on Sandstone and Shale in the Sydney Region, Australian Geomechanics Journal, December 1998.

4.2 Groundwater Investigation

Groundwater seepage was observed during the augering of the borehole BH2. Also standing groundwater levels were measured within the installed groundwater wells. Details of groundwater are summarised in Table 3.

Further groundwater recharge rate test was carried out within the installed groundwater wells.

	Boreholes					
Details	(Groundwater Wells)					
Details	BH1	BH2	BH3	BH4		
	(GW1)	(GW2)	(GW3)			
openado	Not Observed	3.8m	Not Observed	Not Observed		
Seebage	until 5.65m	(RL 71.4m)	until 1.31m	until 1.34m		
Standing groundwater	6.9m	5.8m	4.0m	_		
level on 7/09/2021	(RL 71.0m)	(RL 69.4m)	(RL 69.1m)			
Groundwater Recharge	1 16 x 10 ⁻³	5 04 v 10 ⁻⁴	2 22 v 10-4	_		
Rate (L/s/m ²)	1.10 × 10	5.54 × 10	5.25 × 10			
Hydraulic Conductivity	9 68 x 10 ⁻⁵	1 17 x 10 ⁻⁷	5.15×10^{-8}	_		
K (m/s)	5.00 X 10	1.17 × 10	5.15 × 10			

Table 3: Summary of the Groundwater Details – FES GI

Standing groundwater levels are also subject to a piezometric head at the drilled locations. Therefore, levels may not be representative of natural groundwater conditions of the site.

Further, it should be noted groundwater levels within the site may be subject to seasonal fluctuations, rainfall, prevailing weather conditions and also future developments of the areas and landforms.

4.3 Aggressivity and Salinity Tests

Aggressivity and Salinity tests were carried out on recovered soils and groundwater samples in accordance with Australian and NSW standards, guidelines, and regulations. Results of the Aggressivity tests and Salinity tests carried out are summarised in Table 4 and Table 5 respectively.

Sample ID	Depth (m)	Soil Type	рН	Chloride (mg/kg)	Sulphate As SO₄ (mg/kg)
BH1	2.0	Silty CLAY	5.7	28	81
BH2	3.0	Sandstone	5.2	< 10	55
BH3	1.0	Sandy CLAY	5.6	< 10	55
Piling - Design an	d Installation - AS2	159-2009			
	<u>Clayey Soil</u>	<u>Sandy Soil</u>			
	Non	Mild	> 5.5		< 5,000
Reinforced	Mild	Moderate	4.5 – 5.5		5,000-10,000
Concrete Piles	Moderate	Severe	4.0 – 4.5		10,000-20,000
	Severe	Very Severe	< 4.0		> 20,000
	Non	Non	> 5.0	< 5,000	
Stool Diloc	Non	Mild	4.0 - 5.0	5,000-20,000	
Steer Files	Mild	Moderate	3.0 - 4.0	20,000-50,000	
	Moderate	Severe	< 3.0	> 50,000	

Table 4: Summary of Aggressivity Tests

Table 5: Summary of Groundwater Aggressivity Tests

Sample ID	Depth (m)	Soil Type	рН	Chloride (mg/L)	Sulphate As SO₄ (mg/L)
GW1	_	_	6.9	30	32
Piling - Design an	d Installation - AS2	159-2009			
	<u>Clayey Soil</u>	Sandy Soil			
	Non	Mild	> 5.5	< 6,000	< 1,000
Reinforced	Mild	Moderate	4.5 – 5.5	6,000-12,000	1,000-3,000
Concrete Piles	Moderate	Severe	4.0 - 4.5	12,000-30,000	3,000-10,000
	Severe	Very Severe	< 4.0	> 30,000	> 10,000
	Non	Non	> 5.0	< 1,000	
Steel Diles	Non	Mild	4.0 - 5.0	1,000-10,000	
Steer Plies	Mild	Moderate	3.0 - 4.0	10,000-20,000	
	Moderate	Severe	< 3.0	> 20,000	

Sample ID	Depth (m)	Soil Type	Electrical Conductivity EC (μS/cm)	Factor	Saturated Extracted EC EC _e (dS/m)
BH1	2.0	Silty CLAY	74	7	0.52
BH2	3.0	Sandstone	39	14	0.55
BH3	1.0	Sandy CLAY	42	9	0.38
GW1	-	-	300	1	0.3
Environmental Pl	anning & Assessme	ent Regulation 199	4 Saline		> 4
			Non-S	aline	< 2
			Slightl	У	2 – 4
Dryland Salinity (1993)		Mode	rately	4 – 8
		8-16			
			Highly		> 16

Table 6: Summar	y of Soil Salinity Tests
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5.0 GROUNDWATER MONITORING

Groundwater was monitored over a period from February 2021 to September 2023 to identify the fluctuations of the natural groundwater table. The table identified in **Appendix C** identifies the monitoring that was undertaken over this period.

An analysis of the results indicated that the average groundwater fluctuation across the wells over the period was approximately 2.0m in BH2/GW2 and the minimum standing water level at RL 69.2 and maximum standing water level at RL 71.9, however this was noted to be over a two year period between installation and monitoring.

However, the groundwater seepage was detected within one of the boreholes at the highest point of 3.8m BGL in BH2/GW2 during the FES Geotechnical Investigation.

It is understood that the groundwater is within a semi-confined to confined aquifer based on the geology and that the subsequent drilling and installation has caused the groundwater to measure a significant piezometric head.

6.0 ENVIRONMENTAL SETTINGS

Table	7: Site	Conditions and	Surrounding	Environmental Review	
IaNIC	7. JIC	Conditions and	Junounung		

Site Information			Descr	iptions						
Sensitive Receivers	The nearest s	ensitive huma	n receptors	s are the cu	rrent and future	users of the				
	site, construc	tion workers c	luring the s	site redevel	opment and the	public. The				
	nearest water	course is Berr	y's Creek la	ocated 341n	n south of the site	2.				
Soil Landscape	The Soil Landscape Map viewed on NSW ESPADE indicates that the site is									
Review of NSW Soil and Land	located withir	located within the Glenorie landscape area:								
Information website ESPADE.	Undulating to rolling low hills on Wianamatta Group shales. Local relief 50-80m,									
	slopes 5-20%.	Narrow ridges	, hillcrests	and valleys	. Extensively clear	ed tall open				
	forest (wet sc	lerophyll fores	ts).							
Topography	The topograp	hy viewed on N	ISW ESPAD	E indicated	the following for t	the Glenorie				
Review of NSW Soil and Land	landscapes:									
Information website ESPADE.	Low rolling ar	nd steep hills.	ocal relief	50-120m, s	slopes 5-20%. Cor	ivex narrow				
	(20-300m) ric	lges and hillcr	ests grade	in modera	tely inclined side	slopes with				
	narrow conca	ive drainage li	nes. Mode	rately inclin	ned slopes of 10-2	15% are the				
	dominant lan	dform element	ts.							
Geological Profile	The Geological Map of Sydney (Geological Series Sheet 9130, Scale 1:100,000,									
	1983), publisł	ned by the Dep	artment of	Mineral Re	sources indicates	the residual				
	soils within th	ne site to be ι	ınderlain b	y Triassic A	Age Shale of the V	Wianamatta				
	Group, compr	rising black to	dark grey sl	hale and lar	minate.					
Presence of Acid Sulphate Soils	A review of th	e "Prospect_P	arramatta'	' map indica	ated that the site	is in an area				
Review of NSW Department of Land &	of "No known	occurrences"	of acid sulp	ohate soil m	naterial within the	soil profile.				
Water Conservation (DLWC) Acid										
Sulphate Soil Risk Maps (Edition Two,										
December 1997, Scale 1:250,000.										
Localised Hydrogeology	Number	Location	Depth	SWL	Use	Water				
Review of DPI (Office of Water)		from Site	(m BGL)	(m BGL)		Bearing				
Database.						Zones				
	GW072478	972m NW	180.50	48.00	Domestic	Unknown				
					Bore					

Site Information			Descr	iptions						
	GW108224	900m NE	132.40	35.00	Domestic	Unknown				
					Bore					
Nearest Surface Water Body	The nearest w	atercourse is	Berry's Cre	ek located 3	341m south of the	e site				
Nearest Active Service Station & Dry	Service Station: 1.3km east of the site.									
Cleaner Shop (Google Maps Search)	Dry Cleaner Shop: 400m north-east of the site									
Local Meteorology	The monthly rainfall of the local surrounding area is represented by the data									
(Bureau of Meteorology BOM website)	collected from the BOM rainfall gauge located at the Chatswood Bowling Club,									
	which is locat	ed approxima	tely 2.3km	from St Le	onards. The reco	rds indicate				
	that the mear	n monthly rain [.]	fall in Augu	st (date of t	fieldwork) was 77	'.5mm.				
Regulated Groundwater Resources	The Water Sl	naring Plan fo	or the Grea	ater Metro	politan Region G	roundwater				
	Sources divide	es the east coa	st if NSW in	to 13 grour	ndwater sources,	of which the				
	planned deve	lopment is wit	thin the Sy	dney Centra	al Basin Groundw	ater Source				
	(SCBGS). FES o	classifies the S	CBGS as a p	orous rock	groundwater sou	irce				
Regional Hydrogeology	The most exte	ensive aquifer a	at the site is	the Hawke	sbury Sandstone	aquifer. The				
	horizontal hyd	draulic conduct	tivity of the	Hawkesbu	ry Sandstone is ty	pically in the				
	order of 5x10	⁻⁷ m/sec to 5x1	.0⁻ ⁸ m/sec.							

7.0 GROUNDWATER ASSESSMENT

7.1 Groundwater – Adopted Discharge Criteria

The NSW EPA has endorsed the use of the Groundwater Investigation Levels (GILs) given in the 1999 NEPM 'Schedule B(1) Guideline on the Investigation Levels for Soil and Groundwater' (Amendment 2013) and the water quality trigger levels given in the Australian and New Zealand Guidelines for Fresh and Marine Water Quality (ANZG 2018). These Guidelines provide criteria for:

• Aquatic ecosystems – both marine and fresh waters

The NEPM advises that 'when assessing groundwater contamination, the GILs are to be applied at the point of extraction and as response levels at the point of use, or where there is a likelihood of an adverse environmental effect at the point of discharge'.

For assessing groundwater quality, it is first necessary to assess the potential uses of groundwater downgradient of the site being assessed.

Potential uses of groundwater downgradient of the site include:

- Discharge to water bodies sustaining aquatic ecosystems particularly Fresh Water.
- Extraction of groundwater by local users.

The threshold concentrations presented in the ANZECC (2000) Fresh and Marine Waters Quality Guidelines are considered applicable for the protection of aquatic ecosystems of the receiving waters. As these guidelines apply to receiving waters, it is generally conservative to apply these to groundwater discharging to receiving waters. It is important to note that these are not threshold values at which an environmental problem is likely to occur if exceeded, rather, if the trigger values are exceeded, then further action is required which may include either further site-specific investigations to assess whether or not there is an actual problem or management / remedial action should be undertaken.

It is considered that *Marine water trigger* values are applicable for investigating chemical concentrations in groundwater at the site. The nearest watercourse is Berry's Creek located 341m south of the site. It is understood that the NSW EPA policy is that the trigger values for the protection of 95% of aquatic ecosystems should be used as groundwater assessment criteria when considering moderately or highly disturbed receiving environments. The receiving waters for groundwater at the site are moderately disturbed ecosystems and the ANZG (2018) 95% protection values are therefore considered appropriate groundwater assessment criteria for the site.

Guidelines from the Australian Drinking Water Criteria 2018 have also been included.

Refer to **Appendix E** – Adopted Discharge Criteria.

7.2 Groundwater Installation Methodology

The FES Geotechnical wells were constructed from the 30^{TH of} August 2021 by adopting the following methodology:

- 50mm diameter, Class 18PVC threaded and flush joined casing and 0.45 machineslotted screens were used.
- Coarse, washed sand and gravel was placed in the annulus surrounding the piping to a height of the screen.
- Bentonite pellets were placed in the annulus to form an impermeable plug near the top of the well to prevent surface runoff from entering directly into the well.
- Bentonite pellets were placed in the annulus to form an impermeable plug near the top encountered bedrock.
- A PVC cap was placed on the casing.

 100mm diameter stainless steel flushed covers were used for all well finishes and concreted onto the ground surface.

Well ID	Total Depth	Screening (m)	Surface Level (RL)	Water Bearing	Comment
BH1/GW1-GI	7.75	3.0-8.95	77.9	-	Dry
BH2/GW2	8.65	3.0-8.95	75.2	-	Current
BH3/GW3	7.6	3.0-8.95	73.2	-	Current

Table 8: Summary of Well Construction Details

Table 9: Groundwater Field Results – 2023

Well ID	Date	рН	Electrical	Redox	Dissolved	Temperature	
			Conductivity	Potential	Oxygen	(*C)	
			(EC us/cm)	(ORP	(mg/L)		
				mV)			
BH2/GW2	30/08/2023	3.15	243.5	139	22.7	18.3	
BH3/GW3	30/08/2023	3.24	194.1	98.5	10.4	17.7	

The results of the field parameters measured are summarised as follows:

- pH reading indicated the groundwater is generally acid.
- The EC reading indicated generally fresh water; and
- The redox potential indicated increasing conditions.

7.3 Groundwater Quality

Based on the groundwater sampling completed by FES as part of the FES DSI dated September 2023, the following parameters were outside (above and/or below) the adopted guideline criteria:

• Metals (copper & zinc)

As per the water quality results further action is recommended to be undertaken to improve the quality of the extracted water before discharging into the council stormwater system. Further action includes treatment and retesting water prior to discharge. However, as the basement is not expected to intercept the underlying groundwater table significant amounts of dewatering is not expected.

7.4 Permeability Testing

Pells Class	Bulk Hydraulic Conductivity							
	m/sec							
1	10 ⁻⁹ to 10 ⁻⁸							
2	10 ⁻⁸ to 10 ⁻⁷							
3	10 ⁻⁷ to 5x10 ⁻⁷							
4	5x10 ⁻⁸ to 2x10 ⁻⁷							
5	10 ⁻⁸ to 5x10 ⁻⁸							

Table 10: Summary of Pells Class Hydraulic Conductivity of Hawkesbury Sandstone

The soil mass permeability was assessed using the results of pump-out tests carried out by Foundation Earth Sciences Pty in the FES GI boreholes. On this basis, we have adopted a permeability of 9.68 x 10^{-5} for the residual soils and 1×10^{-7} for the underlying sandstone geology.

The basement is likely to intercept the groundwater table, however significant amounts of dewatering is not expected.

7.5 Seepage Analysis and Results

Using the generalised excavation and shoring geometry together with an idealised subsurface profile and the above permeabilities, seepage analyses were carried out using the 2D finite element computer program which was used in this report. A sensitivity analysis was also undertaken and the effect of varying the permeability of the deeper strata on the inflow rates was examined.

The results of the analysis indicate that an inflow rate int the order of 1.39ML/180 days of constructions phase and 2.64ML/year during operational phase. Drawdown as a result of the dewatering is expected to be negligible if at all present. Based on this calculation and the parameters provided groundwater is unlikely to be identified within the basement.

A water access license is not expected to be required.

7.6 Impact of Dewatering

Based on the results of the dewatering analyses, a detailed assessment of the potential impacts that could arise has been completed. The potential impacts include reducing the groundwater availability to other users, effect on groundwater dependent eco systems and settlements resulting in damage of surrounding buildings, structures and infrastructure as a result of lowering the groundwater levels. The basement is likely to intercept the groundwater table, however significant amounts of dewatering is not expected.

7.7 Impacts on Existing Groundwater Users

Based on preliminary analysis the groundwater level external to the excavation should not be significantly lowered as the as the basement is not expected to intercept the underlying groundwater table. The proposed temporary dewatering will therefore not limit access to the groundwater resource with regards to the Surrounding Buildings, Structures and Infrastructure. Installation of a shoring and internal lowering of the groundwater levels within the excavation could potentially result in some fluctuations of groundwater until the site groundwater flows return to natural equilibrium. This will be mitigated by continual monitoring during construction and further analysis of these areas will be undertaken prior and during construction in order to refine the current dewatering models.

8.0 LICENSING REQUIREMENTS

Dewatering <u>during construction</u> will not require a water licence to account for the groundwater inflow to the basement, since it is less than 3ML / year. T

The predicted maximum long term groundwater inflows to the planned drained basement during the operation phase are expected to be less than 3ML/year. Therefore, this development could be considered as a minor aquifer interference activity which may be exempt from the full extent of the Water Management Act.

9.0 GROUNDWATER IMPACT ASSESSMENT

 Table 11: Minimal Impact Consideration under the Aquifer Interference Policy

AIP – Level 1	Assessment
Water Sharing Plan / Source	Greater Metro Region Groundwater Sources 2011 /
	Sydney Basin Central Groundwater Source
Aquifer	Porous Rock
Category	Less Productive
Water Table	The closest groundwater dependant ecosystem is
	located more than 1km from the subject site.
Water Quality	The proposed development is not expected to lower
	the beneficial use category of groundwater beyond
	40m of the site.

10.0 DEWATERING MONITORING PLAN (CONTINGENCY ONLY)

10.1 General

Temporary groundwater pumping for dewatering within the subject site is predicted to have a minimal effect on groundwater levels in the area. Groundwater levels must, however, be monitored within and outside the excavation (using simple standpipes), and the pumping rate adjusted to maintain groundwater levels to not more than 1m below the base of the bulk excavation level within the excavation pit. External groundwater levels should vary by no more than natural variation from the measured levels.

Where the basement level is found to be within groundwater fluctuation zones then visual inspection of the underlying material is to be undertaken to confirm seepage rates. Based on the depth of the basement we do not envisage significant water flow through the stratum and therefore the dewatering requirements are not expected to be ongoing.

Disposal of pumped groundwater to the local stormwater system is proposed and water quality results available to date, suggest that pumped water should be suitable for discharge, although treatment may be required in some areas.

If water is identified approximately 10,000L – 13,000L of water is proposed to be removed during the dewatering of the basement over the as per the estimated modelling. The estimated duration of dewatering is to be 180 days during construction.

10.2 Groundwater Monitoring

A groundwater level, water quality and dewatering rate monitoring program must be implemented during constructions. The following program is tentatively proposed:

 Weekly monitoring of groundwater levels. The monitoring is to commence prior to dewatering commencing and to continue for a period of at least 2 months following cessation of dewatering.

- Monitoring of discharge water quality to be undertaken weekly, decreasing to monthly after the first four weeks, if groundwater quality is stable. The analytical suite should include as a minimum, Heavy Metals, BTEXN, TRH, PAH, VOC, turbidity, Ph, TDS /TSS, oil & grease and Electrical Conductivity (EC).
- The monitoring results must be provided weekly to the environmental engineer for review.

The final groundwater monitoring program should be developed following assessment of conditions by the authorities.

10.3 Survey Monitoring

A surveying monitoring program must also be implemented. The following program is proposed:

- Establish a benchmark on the site.
- Set up permanent monitoring points on the adjacent building.
- Take baseline level and orientation readings prior to dewatering commencing and thereafter at weekly intervals for a period of at least two months following cessation of dewatering.
- The survey monitoring results must be provided weekly to the geotechnical engineer for review.

10.4 Water Quality Treatment

During the construction process, water needs to be pumped into a holding Tank and a monitoring program needs to be applied. Direct discharge of untreated groundwater may potently cause unlawful environmental harm which is prohibited under the Environmental Protection Act 1994. To ensure that any potential environmental harm is managed correctly and to enable the proponent to demonstrate compliance, regular monitoring of water quality parameters must continue in a manner advised by professionals.

It is recommended that an appropriate filtration system is designed to allow the groundwater to pass through before entering the local system. In addition, the water quality should be sampled before the initial disposal occurs and at regular intervals during the disposal process. The samples should be analysed for Metals, TRH, BTEX, PAH, VOC, TSS, TDS, Turbidity, EC, Oil & Grease and pH as a minimum. Some examples of filtration systems include:

- Sediment Tanks;
- Sediment Tanks supplemented with chemical dosing units to enhance settling rates;
- Media Filtration Systems that can treat a range of recalcitrant contaminants.

It is our understanding that the water comes into the holding tank, the flocculant (eg aluminium sulphate) is added and left-over night to settle. The water quality is then tested and sent to NATA accredited laboratory to determine the suitability for disposal down stormwater. This process is repeated for the duration of the dewatering onsite. Any remaining sediment in the holding tank is to be collected & disposed offsite appropriately.

Foundation Earth Sciences recommends that 'tail' water from the dewatering operation be treated to the *extent practicable* prior to discharging, to meet the adopted discharge water quality criteria.

11.0 CONTINGENCY PLAN

Any exceedances recorded during groundwater or survey monitoring may be interrelated and should not be assessed in isolation.

11.1 Groundwater Level

Should the groundwater level monitoring indicate that the groundwater levels external to the basement are dropping or increasing more than those identified within the seasonal variations, the geotechnical engineer must be informed.

The cause is likely to be higher than estimated permeability of the sands or significant rainfall events. The above would be accompanied by a higher than estimated dewatering rate and the dewatering rate must be measured and provided to the geotechnical engineer.

The survey monitoring interval may need to be increased to assess whether the drawdown/surcharge is causing surrounding buildings and structures to settle.

With respect to pumping, a standby pump and hoses will be kept on site in the event that there is a failure with the installed pumps. If further extra hoses and adaptors to suit the systems are required on site, turnaround time will be within 24 hours of notice.

11.2 Surrounding Buildings and Structures

If the survey monitoring indicates that the adjacent buildings are settling, then we recommend as follows:

- Settlement ≤ 5mm Inform geotechnical engineer and repeat the survey to confirm.
 Work should not stop but proceed with caution and increased vigilance in areas of movement.
- Settlement 5mm to 8mm Inform the geotechnical engineer and repeat the survey to confirm. Work should not stop but proceed with caution and increased vigilance in

areas of movement. The geotechnical engineer, in conjunction with other parties, must analyse the results and attempt to identify the reason for the movement.

 Settlement > 8mm – All work must stop and not recommence until the methodology and monitoring procedures are reviewed and remedial measures or revisions approved by the geotechnical engineer.

Possible causes of movement include excessive groundwater drawdown, deflection of the shoring or subsoil erosion.

Possible remedial measures include groundwater recharge external to the shoring, additional shoring support or blocking leaks through the shoring.

11.3 Groundwater Quality

The monitoring results of the water quality will be regularly assessed by the environmental engineer and an indication of which properties exceed the guideline limits will become evident. Generally the pH can be controlled by dousing whilst turbidity can be controlled by the use of flocculants and settling tanks. Such treatment, if required, will take place prior to discharge into the stormwater pit.

12.0 RECOMMENDATION AND CONCLUSIONS

FES carried out pump tests in boreholes in June 2023. The results of the analysis indicate that an inflow rate int the order of 1.39ML/180 days of constructions phase and 2.64ML/year during operational phase. Drawdown as a result of the dewatering is expected to be negligible if at all present. Based on this calculation and the parameters provided groundwater is unlikely to be identified within the basement.

As the groundwater seepage inflow is less than 3ML/year, we expect that a water access licence will not be required subject to confirmation with WaterNSW. Therefore we recommend that a drained basement is proposed.

During the construction process, if water needs to be pumped into a holding Tank and a monitoring program needs to be applied. It is recommended that an appropriate filtration system is designed to allow the groundwater to pass through before entering the local system. It is our understanding that the water comes into the holding tank, the flocculant (eg aluminium sulphate) is added and left-over night to settle. The water quality is then tested and sent to NATA accredited laboratory to determine the suitability for disposal down stormwater. This process is repeated for the duration of the dewatering onsite. Any remaining sediment in the holding tank is to be collected & disposed offsite appropriately.

Recommendation

Based on the groundwater modelling results provided in this report including the seepage analysis limitations a drained basement is suitable for the development. This report should be read in conjunction with the FES geotechnical report titled "FES (2022) Geotechnical Report 2-10 Berry Road, 14-16 Marshall Avenue & 5-9 Holdsworth Avenue, St Leonards NSW - Ref G546-1 Revision 2.

Thank you for the opportunity of undertaking this work. We would be pleased to provide further information on any aspects of this report.

For and on behalf of Foundation Earth Sciences

Prepared by

ben buckley

Ben Buckley

Director

13.0 LIMITATIONS

The assessment of the sub-surface profile within the proposed development area and the recommendations presented in this report are based on limited information available to date.

The recommendations and advice presented in this report on soil and rock condition is considered to be indicative only as only very limited areas were assessed on site to date. Site inspection by a consulting Geotechnical Engineer or Engineering Geologist are to be undertake when further investigation works are to be carried out to confirm the condition of founding materials in which this geotechnical assessment recommends.

Anecdotal evidence and Information provided by client is assumed to be relevant and to the best of knowledge be appropriate for its interpretation.

There is a possibility that the actual geotechnical and groundwater conditions across the site could differ from the inferred geotechnical assumptions and derivations on which our recommendations are presented in this report. In that case, Foundation Earth Sciences should be contacted for further advise and review of the information provided in this report. Foundation Earth Sciences does not accept any liabilities for the conditions not provided and/or accessible during the preparation of this report. Any ensuring liability resulting from use of this report by third parties cannot be transferred to Foundation Earth Sciences.

14.0 REFERENCES

- 1. Australian Standard AS1726-1993 "Geotechnical Site Investigation".
- Australian Standard AS 1170.4-2007 "Structural Design Actions Part 4: Earthquake actions in Australia".
- 3. Australian Standard AS 2870-2011 "Residential slabs and footings".
- 4. Australian Standard AS 2159-2009 "Piling Design and installation".
- Pells, P.J.N, Mostyn, E and Walker, B F Foundations on Sandstone and Shale in the Sydney Region, Australian Geomechanics Journal, Dec 1998.
- Pells, P.J.N, Douglas D.J, Rodway, B, Thorne C, McManon B.K Design Loadings for Foundations on Shale and Sandstone in the Sydney Region. Australian Geomechanics Journal, 1978.
- Site Investigation for Urban Salinity, Department of Land and Water Conservation 2002.



	FOUNDATION EARTH SCIENCES												
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Method	Water	Well Details	RL (m)	Depth (m)	Graphic Log	Classification Symbol	Material Descrip	ition	Moisture	Consistence	Samples Tests Remarks	Additional Observations	Depth (m)
ADT ADT	Not encountered within the augering		77.8			СН	FILL, gravely silt, low plasticity, gravel, grey-brown-red Silty CLAY, medium to high pla SANDSTONE, fine to medium a interbedded with some clay and weathered, extremely low stren Borehole BH1 continued as cor 5.65m	fine to medium sticity, grey	M M	F St-VSt	SPT 2, 4, 13 N=17 9, 26, Bouncing N > 50	Fill Residual Soils	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
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	FOUNDATION BOREHOLE : BH1 EARTH PAGE 2 OF 3 SCIENCES															
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Method	Water	Well Details	RL (m)	Depth (m)	Graphic Log	Material Description	Weathering	Di Estimated Strength Is(50) SI (MPa) Q Water strength SI (MPa) Q M (MPa) Q (MPa) Q			Defec Spacir (mm) ≈ ∞ [©] 3	Defect bacing (mm) Defect Description ଛୁ ଛୁ ଝୁ ଝୁ		Depth (m)		
				- - - - - - - - - - - - - - - - - - -		Continued from non-corred borehole										- - - - - - - - - - - - - - - - - - -
NMLC			72.3	5.65		SANDSTONE, fine to medium grained, with some shale bands, grey-brown-dark grey	MW	Ш	р. 1 1 1	H H	D A 0.430.82 D A 0.15 0.8 D A 0.530.51	74 68		5.5.5 5.5.5 5.5.5 6.6.6.6 6.6.6.6 6.6.6.6 6.6.6.6 6.6.6.6 6.6.6.6 6.6.6.6.6 6.6.6.6.6.6 6.	72m, B, P, S, 0-5° 76m, B, P, S, 0-5° 55m, B, P, S, 0-5°, 55 30m, B, P, S, 0-5°, 55 30m, B, P, S, 0-5° 30m, B, P, S, 10-15° 30m, B, P, S, 5-10° 32m, B, P, S, 0-5° 39m, B, P, S, 0-5°, Fe 10m, B, P, S, 0-5°, Fe 10m, B, P, S, 0-5°, Fe 30m, J, Ir, R, 70-75°, Fe 30m, J, Ir, R, 70-75°, Fe 30m, B, P, R, 0-5°, Se 30m, B, P, R, 0-5°, Se 30m, B, P, S, 0-5° 30m, B, P, S, 10-15° 30m, B, P, S, 0-5°	
Com	iments:					Weat EW - HW - MW- SW - Fr -	<u>hering</u> Extremely Highly Moderately Slightly Fresh	1	EL - VL - M - H - VH - EH -	Extrem Very Lo Low Mediun High Very Hi Extrem	ely Low D w A 1 gh ely High	- Dia Axi	metral al	F 7 B CS FZ IS SS CZ	- Joint MB - Mechanical Brea - Bedding Plan HB - Handling Break - Clay Seams - Fractured Zone PI - Planar - Infil Seam Ir - Irregular - Sheared Seam Cu - Curved - Crushed Zone St - Stepped	k S - Smooth R - Rough P - Polished Qz - Quartz Fe - Iron Stain

60.2 17.75 BH1 terminated at 17.75m 000000000000000000000000000000000000	CL ST Da B E Method	Mater Mater	T NAME DDRESS Barted : ole Loca ment : Well Details Vell V	CUUI AR 5: _2-1 	NDAI TH NCES dsworth La 0 Berry R 3/2021 Refer to Rig Depth (m) 	ION and Pt d, 14-	y Ltd ATF Holdsworth Land Unit T 16 Marshall Ave & 5-9 Holdsworth Completed :	Ave, St Log Surf Bord MW MW	Leonards N ged By : face RL : ehole Size Estimated Strength	ISW I MM 77.9 77.9 Is(50) Is(50) (MPa) Is(50) (MPa) D A 0.15 1.5 D A 1.090.95 A 1.10.87 A 1.10.87 A 1.10.13 A 1.10 A 1.10 A 1.2 1.71	JOB NUMBE PROJECT:	R: G511 Geotechnical Investigation
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			7 <u>5.2</u> 75.0	0.05 0.20		СН	Brick Pavement, approximate the FILL, gravelly silt, low plasticity, brown-dark grey Silty CLAY, medium to high pla red mottling	nickness of 50mm fine gravel, dark sticity, grey with	M	F St-VSt		Fill Residual Soils	- - - 1
Ŀ			74.0	1.20		CS	Sandy CLAY, medium to high p medium grained sand, grey-red	lasticity, fine to -brown	M	St-VSt	SPT 3, 6, 9 N=15		
AD			72.7	2.50 · · · · · · · · · · · · · · · · · · ·			SANDSTONE, fine to medium g interbedded with some clay and weathered, extremely low stren	grained, I shale, extremely gth, yellow-grey	M-W			Bedrock	
				4								Seepage from 3.8m to 4.0m	
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Method	Water	Well Details	RL (m)	Depth (m)	Graphic Log	Material Description		Weathering	E ; d;	Stren Stren	ated gth ⊥∃i	ls ₍₅₀₎ (MPa) ⊞	RQD %	Def Spa (m ରୁ ନ୍ତୁ	ect cing m)	Defect Description	Depth (m)
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Date	e St	tarted :	1/09/	2021		Completed : 2/09/2021	Lo	bgg	jed By : _	RL			Checked I	By: MM	
Bor	eho	le Loca	tion :	Refer to	Site P	lan	Sເ	urfa	ace RL : _	73.2			Datum : _	m AHD	
Equ	ipn	nent : _	Drilling	Rig	1		Bo	ore	hole Size	: <u>100n</u>	nm		Slope :	·90°	
Method	Water	Well Details	RL (m)	Depth (m)	Graphic Log	Material Description	Weathering	ū	Estimated Strength	ls ₍₅₀₎ (MPa)	RQD %	Defect Spacing (mm)	Defect I	Description	Depth (m)
NMLC						Continued from non-cored boreho SHALE, interbedded with clay and sandstone, fine to medium graine brown-red-grey SHALE, interbedded with sandstone, fine to medium graine dark grey-brown SANDSTONE, fine to medium grained, with some shale bands, light grey-grey	ole d, EW d, HW d, HW SW			D A 1.542.26 D A 0.01 0 D A 0.380.66 D A 0.4 1.41 D A 0.4 1.41 D A 0.57 0.52			4.43m, B, P, S, 0.5° 4.46m, B, P, S, 0.5° 4.46m, B, P, S, 0.5° 4.71m, J, Ir, R, 0.5° 4.86m, B, P, S, 0.5° 5.00m, B, P, S, 0.5° 5.00m, B, P, S, 0.5° 5.00m, B, P, S, 0.5° 5.00m, B, P, S, 0.5° 5.35m, B, P, S, 0.5° 5.35m, B, P, S, 0.5° 5.56m, B, P, S, 0.5° 5.64m, B, P, S, 0.5° 6.32m, B, P, S, 0.5° 6.32m, B, P, S, 0.5° 6.32m, B, P, S, 0.5° 6.56m, EW, 10mm 6.80m, B, P, S, 0.5° 6.84m, B, P, S, 0.5° 6.84m, B, P, S, 0.5° 7.20m, HB 7.14m, HS 7.56m, B, P, S, 0.5° 7.76m, J, Ir, S, 0.15° 7.76m, J, Ir, S, 0.15° 7.76m, J, P, S, 0.5° 8.42m, B, P, S, 0.5° 8.45m, B,		
Comm	ents:					y y H M S	<u>Neathering</u> EW - Extremel W - Highly WW - Moderate SW - Slightly	y ely	EL - Extrem VL - Very Lo L - Low M - Medium H - High	elyLow D bw A n	- Dia Axi	metral	J - Joint M B - Bedding Plan H CS - Clay Seams FZ - Fractured Zone F IS - Infill Seam	/IB - Mechanical Break -IB - Handling Break 21 - Planar r - Irregular	S - Smooth R - Rough P - Polished Qz - Quartz
						F	ı - ⊢resh		v⊓ - very Hi EH - Extrem	ely High			CZ - Crushed Zone S	St - Stepped	ie - non Stain

C∟	IEN	F E S T NAME:		NDAT TH NCES dsworth La	ION	y Ltd ATF Holdsworth Land U	nit Trust		JI	ob number	BOREHOLE PAGI	: BH3
SI	EA	DDRESS	3 : <u>2-1</u>	0 Berry R	d, 14-	16 Marshall Ave & 5-9 Holdsv	vorth Ave, St	Leonards N	<u>SW</u> P	ROJECT: _(Seotechnical Investigation	
Da	te S	tarted :	1/09/	2021		Completed : 2/09/2021	Log	ged By : _F	RL		Checked By : _ MM	
Во	reho	ole Loca	tion :	Refer to	Site P	lan	Sur	face RL :	73.2		Datum : _m AHD	
Eq	uipn	nent: _	Drilling	Rig			Bor	ehole Size :	: <u>100m</u> i	m	Slope :90°	
Method	Water	Well Details	RL (m)	Depth (m)	Graphic Log	Material Description	Weathering	Estimated Strength 쿄弓₋≥ェ롯Ђ	Is ₍₅₀₎ (MPa)	Defect Spacing (mm) 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Defect Description	Depth (m)
NMLC				- - 11 - - - - - - - - - - - - - - - -		SANDSTONE, fine to medium grained, with some shale band light grey-grey (continued)	s, SW		_D A_ 1.4 1.75 ⁻ _D A_ 1.711.89_	89 75	9.14m, MB 9.54m, CS, 10mm 9.62m, CS, 10mm 9.66m, B, P S, 0-10° 9.71m, B, P S, 0-5° 9.77m, B, P S, 0-5° 9.00m, B, P S, 5-10° 10.00m, HB 10.00m, HB 10.00m, EW, 10mm 10.18m, B, P, S, 0-5° 10.55m, MB 10.85m, B, P S, 0-5° 10.55m, MB	1_
is (updated on zu/u4/zu/u)						BH3 terminated at 11.27m			1.711.89_		10.55m, MB 10.86m, B, P, S, 0.5* 11.00m, HB 11.9m, B, P, S, 0.5* 11.22m, B, S, 0.5* 11.27m, MB 11.27m, MB 11.27	
				20	_			비수 - 호ェ 한 보		88898	3	2
	ments:						Weathering EW - Extremely HW - Highly MW - Moderately SW - Slightly Fr - Fresh	EL - Extremeț VL - Very Low L - Low M - Medium H - High VH - Very Higt EH - Extremet	ly Low D - v A h ly High	Diametral Axial	J - Joint MB - Mechanical Break B - Bedding Plan HB - Handling Break CS - Clay Seams FZ - Frachured Zone PI - Planar IS - Infill Seam Ir - Irregular SS - Sheard Seam Cu - Curved CZ - Crushed Zone St - Stepped	S - Smooth R - Rough P - Polished Qz - Quartz Fe - Iron Stain

			FOUN EART SCIEI	IDA H NCE	TIOI S	Ν					BOREHOLE : E PAGE 1	3H4 OF 3
CL SI	.IEN ⁻ TE A	t nam .ddre:	E: <u>Hold</u> SS: <u>2-10</u>	sworth) Berry	Land I	Pty Ltd ATF Holdsworth Land Unit Tru 4-16 Marshall Ave & 5-9 Holdsworth A	st .ve, St Leonards NS	SW	JOB N PROJI	UMBER: _(G511 echnical Investigation	
Da Bo	ite S oreho	tarted ble Loc	: _7/09/2	2021 Refer	to Site	_ Completed : <u>7/09/2021</u> Plan	_ Logged By : _R _ Surface RL : _7	RL 72.1			Checked By : _MM Datum : _m AHD	
Eq	luipr	nent :	Drilling	Rig			_ Borehole Size :	_100	mm		Slope :90°	
Method	Water	RL (m)	Depth (m)	Graphic Log	Classification Symbol	Material Descriptior		Moisture	Consistence	Samples Tests Remarks	Additional Observations	Depth (m)
	ering	-	-			FILL, silty clay, low to medium plasticity	, brown-dark brown	м	F		Fill	-
ΗA	within the aug	71.7	0.40 1		СН	Sandy CLAY, medium to high plasticity,	light brown-orange	М	St		Residual Soils	
Earth Sciences (Updated on 20/04/2020)	Not encountered	70.8	1.34 2 3 3 3 3 4 5 5 6 6 6 6 7 <t< th=""><th></th><th></th><th>Borehole BH4 continued as cored hole</th><th>rom 1.34m</th><th></th><th></th><th></th><th>Hand Auger retusal</th><th>2 2 3 3 3 4 4 5 5 5 5 7 7 7 7 7 7 7 7 7 7 7 7 7 7</th></t<>			Borehole BH4 continued as cored hole	rom 1.34m				Hand Auger retusal	2 2 3 3 3 4 4 5 5 5 5 7 7 7 7 7 7 7 7 7 7 7 7 7 7
© Foundation E	nments:							D - Dry M - Moist W - Wet	VS S F St VSt H	- Very Soft V - Soft L - Firm M - Stiff D - Very Stiff V - Hard	L - Very Loose - Loose ID - Medium Dense - Dense D - Very Dense	

			FOL EAR SCII	JNI RTH EN		TION S	ruct							BOREHOLE PAC	: BH4 Ge 2 OF 3
SI		DDRE	SS: _2	-10	Berry	Rd, 14-16 Marshall Ave & 5-9 Holdsworth	Ave, St	t Le	eonal	rds N	<u>ISW</u> F	PRO	JECT:	Geotechnical Investigation	
Da Bo	te Si reho	tarted ble Loc	: <u>7/0</u>	9/20 : _F	21 Refer	to Site Plan	Loç Sur	gge rfac	ed By ce R	y:	RL 72.1			Checked By :MM Datum :m AHD	
Eq	uipn	nent :	Drillin	ng Ri	ig		Bor	reh	ole	Size	: <u>100m</u>	m		Slope :90°	
Method	Water	RL (m)	Dept (m)	th)	Graphic Log	Material Description	Weathering	E ;	Estim Stren ⊰ _ ≥	ated igth ⊥∃⊞	Is ₍₅₀₎ (MPa)	RQD %	Defect Spacing (mm)	Defect Description	Depth (m)
		70.8	1.34	- - 1 -		Continued from non-cored borehole	EW								
				2		grey-brown, with some clay bands					D A 0.460.42	0			2
		69.2	2.90	3		SANDSTONE, interbedded with shale, fine to medium grained, grey-brown-red-light grey) HW				DA 0.44 0.54	20		2.90m, B, P, S, 0.5° 2.97m, HB 3.14m, B, P, S, 0.5° 3.35m, B, P, S, 0.5° 3.35m, B, P, S, 0.5° 3.48m, EW, 10mm 3.66m, J, P, R, 40-50° 3.71m, B, P, R, 0.5° 3.82m, EW, 40mm 3.92m, B, P, R, 0.5° 3.92m, B, P, R, 0.5° 4.00m, MB	<u>.</u>
NMLC				5							D A 0.430.31	30		4.37m, B, P, S, 15-20" 4.50m, B, P, S, 5-10" 4.69m, CS, 60mm 4.69m, CS, 20mm 4.91m, B, P, S, 0-5" 4.95m, B, P, S, 0-5" 5.00m, HB 5.04m, B, P, S, 0-5" 5.04m, B, P, S, 0-5" 5.13m, B, P, S, 0-5" 5.17m, B, P, S, 0-5" 5.26m, B, P, S, 0-5" 5.21m, B, P, S, 0-5"	<u>.</u>
		65.9	6.20	<u>-</u> - 7		SANDSTONE, fine to medium grained, with some shale bands, light grey-grey	MW- SW				0.431.22	61		5.37m, B, P, S, 0-5" 5.37m, B, P, S, 0-5" 5.43m, B, P, S, 0-5" 5.43m, B, P, S, 0-5" 5.43m, B, P, S, 0-5" 5.55m, MB 5.58m, B, Ir, S, 0-5" 5.64m, B, P, S, 0-5" 5.73m, B, P, S, 0-5" 5.73m, B, P, S, 0-5" 6.00m, B, P, S, 0-5"	<u> </u>
2020)				- - 8 -							DA 0.671.11	73		6.03m, B, P, S, 0-5° 6.07m, B, Ir, S, 0-10° 6.08m, B, P, S, 0-5° 6.11m, B, P, S, 0-5° 6.13m, B, P, S, 0-5° 6.33m, B, P, S, 0-5° 6.33m, B, P, S, 0-5° 6.44m, B, P, S, 0-5° 6.46m, B, P, S, 0-5° 6.67m, B, P, S, 0-5° 6.77m, B, P, S, 0-5° 6.77m, B, P, S, 0-5°	<u>8</u>
LANA (Dhated on FANA				9							D A 0.390.47 D A 1.580.97	53 30	<u></u> <u></u>	7.00m, MB, S,	
	ments:			10		Wei EW HW SW Fr	athering - Extremely - Highly - Moderately - Slightly - Fresh	 	EL - VL - L - H - EH -	Extreme Very Lo Low Medium High Very Hig Extreme	ely Low D w A gh gh	- Diar Axia	netral	B - Joint MB - Mechanical Brea B - Bedding Plan CS - Clay Seams FZ - Fractured Zone PI - Planar IS - Infill Seam Ir - Irregular SS - Sheared Seam Cu - Curved CZ - Crushed Zone St - Stepped	k S - Smooth R - Rough P - Polished Oz - Quartz Fe - Iron Stain

			FOUN EART SCIEN	DA H ICE	TION S							BOREHOLE	E : B GE 3 C	H4 DF 3
CL	IENT	NAM	E: Holds	worth	Land Pty Ltd ATF Holdsworth Land U	Jnit Tru	ist		、	JOE		R: G511		
SIT	ΈA	DDRE	SS : <u>2-10</u>	Berry	Rd, 14-16 Marshall Ave & 5-9 Holdsv	worth A	Ave, St	Leonards N	ISW	PRC	JECT: _(Geotechnical Investigation		
Da	te Si	tarted	: 7/09/20	021	Completed : 7/09/2021		_ Log	ged By : _	RL			Checked By : _MM		
Во	reho	le Loc	cation : _	Refer	to Site Plan		_ Sur	face RL : _	72.1			Datum : AHD		
Eq	uipn	nent :	Drilling F	Rig			_ Bor	ehole Size	: <u>100n</u>	nm		Slope :90°		
Method	Water	RL (m)	Depth (m)	Graphic Log	Material Description		Weathering	Estimated Strength ⊐ ⊃ -	Is ₍₅₀₎ (MPa)	RQD %	Defect Spacing (mm)	Defect Description		Depth (m)
NMLC			-		SANDSTONE, fine to medium grained, some shale bands, light grey-grey (cont	with inued)	MW- SW		_D A_	53	أمل	8.56m, B, Ir, S, U-10 8.68m, B, P, S, 0-5° 8.75m, B, P, S, 0-5° 8.77m, CS, 20mm 8.83m, B, P, S, 0-5°		
		61.5 	10.57 - - - - - - - - - - - - - - - - - - -		BH4 terminated at 10.57m				Ţ.231.9Ē	5		 8.88m, B. P. S. 0-5" 9.92m, J. Ir, S. 80-90" 9.03m, B. Ir, S. 0-10" 9.03m, B. P. S. 0-5" 9.10m, C. S. 60mm 9.10m, C. S. 60mm 9.24m, B. P. S. 0-5" 9.27m, MB, P. S. 0-5" 9.40m, B. P. S. 0-5" 9.47m, B. P. S. 0-5" 9.62m, B. P. S. 0-5" 9.67m, B. P. S. 0-5" 10.10m, B. P. S. 0-5" 10.10m, B. P. S. 0-5" 10.27m, B. P. S. 0-5" 10.32m, B. P. S. 0-5" 10.33m, B. P. S. 0-5" 10.48m, B. P. R. 20-30" 10.57m, MB 		$\begin{array}{c} - & - \\ 11 \\ - & - \\ 12 \\ - & - \\ 12 \\ - & - \\ 13 \\ - & - \\ 16 \\ - & - \\ 16 \\ - & - \\ 16 \\ - & - \\ 16 \\ - & - \\ 18 \\ - \\ - \\ 19 \\ - \\ - \\ - \\ 19 \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ $
<u> </u>			20					EH H H L L L L L L L L L L L L L L L L L			20 60 540 620	60		20
Com	ments:					Weather EW - E HW - H MW - M SW - S Fr - F	ering Extremely lighly loderately lightly resh	EL - Extreme VL - Very Lo L - Low M - Medium H - High VH - Very Hig EH - Extreme	elyLow D w A ı gh ∋lyHigh	- Dia Ax	ametral ial	* MB - Mechanical Bre B - Bedding Plan HB - Handing Break CS - Clay Seams FZ - Fractured Zone PI - Planar IS - Infill Seam Ir - Irregular SS - Sheared Seam Cu - Curved CZ - Crushed Zone St - Stepped	ak S - Sm R - Rou P - Pol Qz - Qu Fe - Iror	iooth ugh lished artz n Stain

SAMPLE ID	RL for for location	DATE	SWL/m (BGL)	RL for Water Level	DATE	SWL/m (BGL)	RL for Water Level	DATE/TIME	SWL/m (BGL)	RL for Water Level
			Sep-21			Jun-23			Jul-23	
BH1/GW1	77.9	30/08/2021	6.9	71	13/06/2023	6.8	71.1	12/07/2023	6.9	71
BH2/GW2	75.2	30/08/2021	5.8	69.4	13/06/2023	3.3	71.9	12/07/2023	3.5	71.7
BH3/GW3	73.2	30/08/2021	4	69.2	13/06/2023	2.8	70.4	12/07/2023	3	70.2
		-	-	-						
SAMPLE ID	RL for for location	DATE	SWL/m (BGL)	RL for Water Level	DATE	SWL/m (BGL)	RL for Water Level	DATE/TIME	SWL/m (BGL)	RL for Water Level
			Aug-23			Aug-23			Sep-23	
BH1/GW1	77.9	3/08/2023	6.9	71	30/08/2023	6.8	71.1	8/09/2023	6.7	71.2
BH2/GW2	75.2	3/08/2023	3.4	71.8	30/08/2023	3.3	71.9	8/09/2023	3.6	71.6
BH3/GW3	73.2	3/08/2023	3.2	70	30/08/2023	2.8	70.4	8/09/2023	3.1	70.1
		-	-	-						

Table 1: Monitoring of Groundwater Levels at St Leonards

Table A1

			Hea	vy Met	als (Di	ssolved)			TF	RH				BTEX						PAH			
FOUNDATION EARTH SCIENCES	ARSENIC	CADMIUM	CHROMIUM	COPPER	LEAD	MERCURY	NICKEL	ZINC	F1 (C ₆ -C ₁₀)	F2 (>C ₁₀ -C ₁₆)	BENZENE	TOLUENE	ETHYL BENZENE	M/P-XYLENE	O-XYLENE	NAPHTHALENE	TOTAL-XYLENE	BENZO(A)PYRENE	ANTHRACENE	PHENANTHRENE	FLUORANTHENE	NAPHTHALENE	
Limit of Resolution (LOR)	1	0.1	1	1	1	0.05	1	1	10	50	1	1	1	2	1	1	-	1	1	1	1	1	
Discharge Water Criteria																							
Based on ANZ (2018) + ANZECC 2000 + Drinking Water																							
Default Trigger Values South East Oz - Marine																							6.5
Fresh Water Trigger Values (95%)	24/13	0.2	1	1.4	3.4	0.06	11	8	-	-	950	-	-	200	350	-	-	-	-	-	-	16	
Fresh Water Trigger Values (95%) -low reliability												180	80					0.1	0.01	0.6	1	-	
Marine Water		0.7	4.4	1.3	4.4	0.1	7	15			500											50	
NHMRC 2018 Drinking Water																							
Default Trigger Values South Fast Oz - Marine																							







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Note

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PTW takes no responsibility for external building elements. Anything connected with any design, materials selection, construction or installation of any cladding, facade or external building element must be checked by and remains the responsibility of others, including suitably qualified experts as may be required.

Rev Amendment

B ISSUE FOR DA SUBMISSION A ISSUE FOR COORDINATION By Chk* Date JY LG 24/03/23 JY LG 03/02/23 *Registered Architect

LGU Lilian Gu

Consultants

NSW Arch 8013

AREA 15



13

Key Plan:

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ptw.com.au	

AREA 13



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Project PA030465

14-16 Marshall Avenue, 5-9 Holdsworth Avenue & 2-10 Berry Road, ST Leonards Status

8m Title DA DRAWINGS SECTION BLDG 13-15

Drawing Number

DA-D120010 B

Revision